

## Note

# Formation of Ganymede's grooved terrain by convection-driven resurfacing



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## ABSTRACT

The heat flux and strain rate inferred for grooved terrain formation on Ganymede can be produced in a convecting ice shell 10–100 km thick with weak near-surface ice. Smooth linear grooves may have formed by convection-driven lithospheric spreading and long-wavelength compressional folds may form atop convective downwellings, and would possibly be detectable with mapping from ESA's upcoming Jupiter-Icy Moon Explorer Mission.

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## 1. Introduction

Over half the surface of Ganymede, Jupiter's largest satellite, is covered in grooved terrain, composed of 10–100 km wide linear and polygonal swaths (Collins et al., 1998) of sub-parallel ridges and troughs (Murchie et al., 1986; Pappalardo, 1998). The ridge and trough spacing is  $\sim 7$  km, though they are often subdivided by narrower grooves 100 m – 1 km wide (Pappalardo, 1998). A subset of groove lanes, which we refer to as “subdued grooves”, have straight margins and relatively constant widths over large distances (Head, 2002) and are characterized by subdued light material (Patterson et al., 2010).

Grooved terrain is thought to have formed during an era of global surface expansion (Smith, 1979) resulting from satellite differentiation (Squyres, 1980) or from the melting of the ice I shell when Ganymede entered a possible Laplace-like resonance with Europa and Io (Showman et al., 1997; Bland et al., 2009). Subparallel grooves may form by tilt-block style normal faulting (Pappalardo, 1998) due to tensional stresses in the lithosphere.

Convection in the ice shell has been suggested as a driving mechanism for grooved terrain formation (Lucchitta, 1980; Parmentier et al., 1982), because it can operate globally and generate zones of intense local deformation (Shoemaker et al., 1982). Head (2002) argued that subdued grooves form in a similar way to extensional bands on Europa, which likely form by a convection-driven midocean rift-type mechanism (Prockter et al., 2002).

Previous work argues that convective stresses were not strong enough to drive surface deformation on Ganymede (Squyres and Croft, 1986); convective plumes were thought to be confined below a “stagnant lid”, a highly viscous layer of ice which inhibits resurfacing (Solomatov, 1995). However, if the near-surface has a yield stress comparable to the thermal buoyancy stresses from convection, plumes can approach the surface, leading to deformation and efficient heat transport (Trompert and Hansen, 1998; Tackley, 2000; Solomatov, 2004; Showman and Han, 2005). This style of “sluggish lid” convection may be occurring beneath the active South Polar Terrain (SPT) of Enceladus (Barr, 2008). The observed heat flow and surface age of the Enceladus SPT are consistent with heat flows and deformation rates associated with sluggish lid convection (Barr, 2008; Han et al., 2012).

On Ganymede, surface conditions may also have been consistent with sluggish lid convection. Models of flexural uplift estimate a heat flux of 100–200 mW m<sup>-2</sup> for grooved terrain (Nimmo et al., 2002), and a heat flux of 60–80 mW m<sup>-2</sup> for the adjacent dark terrain (Nimmo and Pappalardo, 2004). While heat flow estimates based on flexure are somewhat uncertain, independent estimates based on models of groove terrain formation by extensional necking predict a similar heat flux of  $\sim 50$  mW m<sup>-2</sup> (Bland et al., 2010). Extensional necking models also predict strain rates between  $10^{-16}$  and  $10^{-13}$  s<sup>-1</sup> for high-relief grooved material (Dombard and McKinnon, 2001; Bland and Showman, 2007), close to strain rates inferred from folds observed in between the tiger stripes of the SPT (Barr and Preuss, 2010).

Here, we simulate solid-state convection in an ice shell with a weak upper surface to show that the heat flow and deformation rates arising from sluggish lid convection are consistent with the

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conditions inferred for grooved terrain formation. Subdued grooves may be areas where convection drove complete lithospheric separation, whereas other grooves may form in response to subsurface flow above a convective upwelling (Lucchitta, 1980).

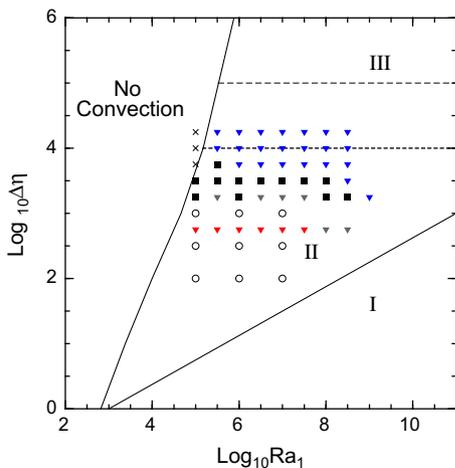
## 2. Methods

We use the two-dimensional Cartesian finite element model CITCOM (Moresi and Solomatov, 1995) to simulate solid state convection in Ganymede’s ice shell. We explore a wide range of ice shell conditions by varying the basal Rayleigh number,  $Ra_1$ , which governs the vigor of convection and is related to  $D$ , the ice shell thickness,

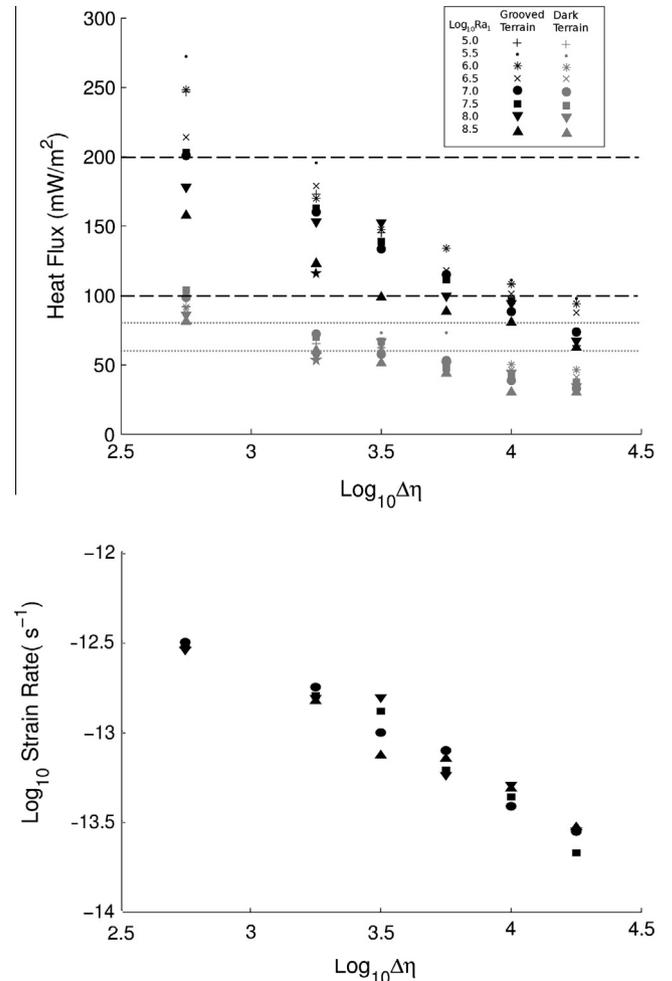
$$Ra_1 = \frac{\rho g \alpha \Delta T D^3}{\kappa \eta_1}, \quad (1)$$

with ice density  $\rho = 1000 \text{ kg m}^{-3}$ , surface gravity  $g = 1.4 \text{ m s}^{-2}$ , coefficient of thermal expansion  $\alpha = 10^{-4} \text{ K}^{-1}$ , basal viscosity  $\eta_1$ , thermal diffusivity  $\kappa = 10^{-6} \text{ m}^2 \text{ s}^{-1}$ , and  $\Delta T = 150 \text{ K}$  is the difference between the temperature at the base (260 K) and the surface (110 K) of the ice shell. With these parameters,  $Ra_1 = 2.1 \times 10^8 (D/100 \text{ km})^3 (10^{14} \text{ Pa s}/\eta_1)$ .

We use a simple temperature dependent viscosity (Solomatov and Moresi, 2000),  $\eta(T) = \eta_0 \exp(-\gamma T)$ , where  $\gamma = \theta/\Delta T$ ,  $\theta = \ln(\Delta\eta)$ , and  $\Delta\eta = \eta_0/\eta_1$  is the viscosity contrast between ice at the surface ( $\eta_0$ ), and ice at the base of the shell. On Ganymede, the  $\Delta\eta$  predicted for an ice shell deforming by Newtonian volume diffusion is very large (Goldsby and Kohlstedt, 2001), and convection is predicted to occur in the stagnant lid regime. However, the effective viscosity of the surface can be dramatically reduced if convective stresses exceed the lithospheric yield stress (Solomatov, 2004), leading to so-called “sluggish lid” convection. Previous work shows that sluggish lid behavior can occur on Enceladus and Europa for surface yield stress  $<100 \text{ kPa}$  (Showman and Han, 2005; Barr, 2008; O’Neill and Nimmo, 2010). Here, we limit the effective viscosity of surface by imposing a low  $\Delta\eta$ , which is the simplest



**Fig. 1.** Values of Rayleigh number ( $Ra_1$ ) and viscosity contrast ( $\Delta\eta$ ) explored in this study. Black squares represent simulations which successfully match heat flux estimates based on flexure for grooved terrain and dark terrain at strain rates inferred from models of extensional necking. Inverted triangles show simulations that do not meet these criterion, with blue showing those with a heat flow that is too low, gray showing those with an average strain rate exceeding  $10^{-13} \text{ s}^{-1}$ , and red showing simulations with an average heat flux exceeding  $200 \text{ mW m}^{-2}$  in regions of extension. “x” symbols show simulations that do not convect and empty circles represent simulations run for the Enceladus SPT by Barr (2008). Lines indicate the boundaries between convective regimes: isoviscous (I), sluggish lid (II), and stagnant lid (III). Dashed lines indicate gradual transition from sluggish lid regime to stagnant lid regime.

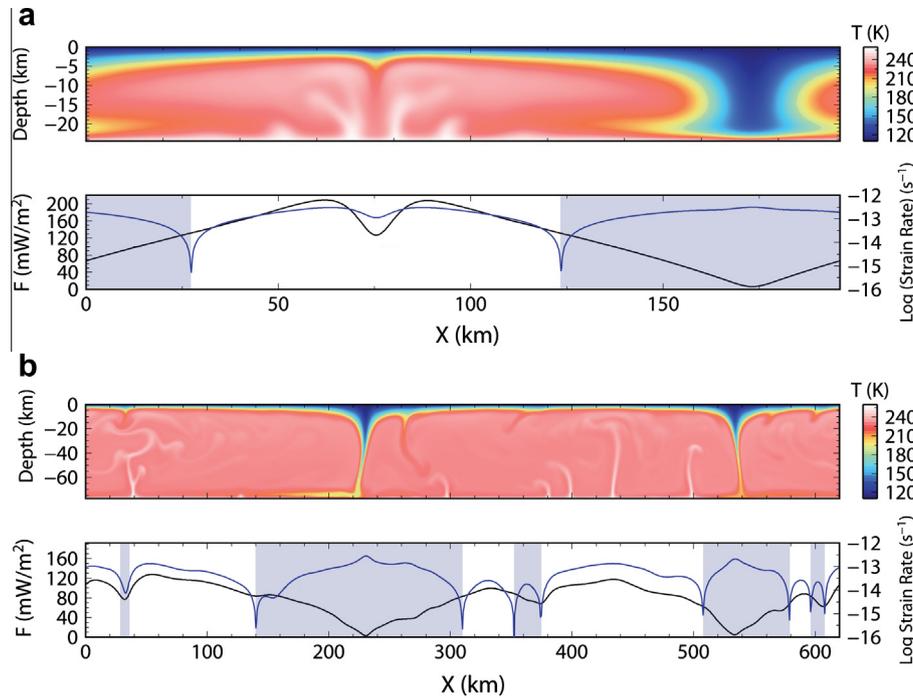


**Fig. 2.** (top) Heat flux of convection simulations plotted as a function of viscosity contrast. Basal Rayleigh numbers of  $\log_{10}(Ra_1) = (5.0, 5.5, 6.0, 6.5, 7.0, 7.5, 8.0, 8.5)$  are plotted with the symbols, (indicated in legend), plus, dot, asterisk, cross, circle, square, inverted triangle and upright triangle, respectively. Star symbols represent one simulation for  $Ra_1 = 10^9$ . Black symbols represent average heat flux in regions of extension, and gray symbols show the average heat flux in regions of contraction. Black dashed lines show estimated heat flux for grooved terrain. Gray dotted lines show estimate heat flux for dark terrain. (Bottom) Surface strain rate of convection simulations plotted as a function of viscosity contrast. Basal Rayleigh numbers represented by same symbols as above, although many overlap and are not visible.

way of mimicking the effect of brittle surface ice with a low yield stress (Barr, 2008). We use  $\eta_1 = 10^{14} \text{ Pa s}$ , for an ice grain size  $\sim 0.1 \text{ mm}$  (Barr and McKinnon, 2007).

We simulate convection for  $\Delta\eta$  between  $10^{2.75} - 10^{4.25}$ , close to the boundary between the sluggish lid regime and stagnant lid regime,  $\Delta\eta \sim 10^4 - 10^5$  (Solomatov, 1995). We model convection in an  $8 \times 1$  domain, with  $512 \times 64$  elements, with periodic boundary conditions at the sides to minimize edge effects. We use a basally heated ice shell because the spatial distribution of tidal dissipation in a convecting ice shell is not fully understood (Han and Showman, 2010). Additionally, surface deformation rates and heat flow are likely insensitive to the precise mode of heating (Solomatov and Moresi, 2000). We allow all our simulations to reach a steady state, then measure how strain rate and heat flux vary at the surface.

The convective heat flux,  $F = \frac{k\Delta T}{D} Nu$ , where  $k = 3.3 \text{ W m}^{-1} \text{ K}^{-1}$  is the thermal conductivity and  $Nu$  is the Nusselt number, which describes the efficiency of convective versus conductive heat transport. The strain rate is approximated by  $\dot{\epsilon} = (\partial v_{xsf}/\partial x)$ , where  $v_{xsf}$



**Fig. 3.** Temperature fields of convection simulations with the corresponding surface heat flux (black) and strain rate (blue) plotted below. Shaded areas indicate regions of surface contraction interpreted as dark terrain (a) Simulation with  $Ra_1 = 10^6$  and  $\Delta\eta = 10^{3.25}$ , corresponding to  $D = 25$  km. A groove lane 150 km wide forms at  $x = 75$  km. (b) Simulation with  $Ra_1 = 10^8$  and  $\Delta\eta = 10^{3.5}$ , corresponding to  $D = 80$  km. Groove lanes form near  $x = 50$  km (80 km wide) and  $x = 450$  km (100 km wide). Narrower groove lanes also form near  $x = 10$  km,  $x = 330$  km and  $x = 590$  km.

is the horizontal velocity at the surface. Simulations successfully match the inferred conditions for grooved terrain formation if regions of surface extension have an average heat flux of  $100\text{--}200\text{ mW m}^{-2}$ , regions of compression have a heat flux of  $60\text{--}80\text{ mW m}^{-2}$  predicted for dark terrain, and surface strain rates are  $10^{-13}\text{--}10^{-16}\text{ s}^{-1}$ .

### 3. Results

For  $Ra_1 = 10^5\text{--}10^{8.5}$  and  $\Delta\eta = 10^{3.25}\text{--}10^{3.75}$  (see Fig. 1), convection can match the heat flux inferred for both grooved terrain and dark terrain, at surface strain rates suggested by extensional necking models. Given a basal viscosity of  $10^{14}$  Pa s, ice shell thicknesses of  $8\text{--}110$  km and an effective surface viscosity  $\eta_0 < 10^{18}$  Pa s are conducive to forming grooved terrain in a convecting ice shell. This corresponds to a surface yield stress  $\sigma_{sy} < 60$  kPa for  $\eta_0 \sim \sigma_y(z)/2\dot{\epsilon}$ , with  $\sigma_y(z) = \sigma_{sy} + \mu\rho gz$ , coefficient of friction  $\mu = 0.1$ ,  $\dot{\epsilon} = 10^{-13}\text{ s}^{-1}$  and depth  $z = 1$  km, close to elastic thickness estimates for grooved terrain (Nimmo et al., 2002).

Fig. 2 shows the surface strain rate and heat flow in regions of extension and contraction as a function of  $\Delta\eta$ . The average heat flux is independent of  $Ra_1$ , however, lower Rayleigh numbers result in larger differences in heat flux over regions of extension and contraction; more vigorously convecting ice shells generate more uniform surface heat flows. For  $\Delta\eta \geq 10^4$  the surface heat flux is below that inferred from models of flexure, but may be consistent with estimates based on models of extensional necking. Surface strain rates are significant even for  $\Delta\eta > 10^{3.75}$ , suggesting that convection-driven resurfacing can occur on the boundary between the stagnant lid and sluggish lid regimes. For  $\Delta\eta \leq 10^{3.25}$  the average surface strain rate exceeds the range inferred from extensional necking models, however strain rates as high as  $10^{-12}\text{ s}^{-1}$  have been inferred for European bands (Stempel et al., 2005), which may be a more appropriate constraint for subdued grooves.

Fig. 3a shows the temperature field, and the variation of  $F$  and  $\dot{\epsilon}$  on the surface, of a convection simulation with  $Ra_1 = 10^{6.5}$  and  $\Delta\eta = 10^{3.25}$ , corresponding to  $D = 25$  km. Regions undergoing extension are interpreted as sites of groove formation and are  $\sim 100$  km wide, with an average heat flux of  $170\text{ mW m}^{-2}$  and strain rates of  $10^{-14}\text{--}10^{-13}\text{ s}^{-1}$ . Outside this region, the average heat flux is  $70\text{ mW m}^{-2}$ . Fig. 3b shows a case with  $Ra_1 = 10^8$  and  $\Delta\eta = 10^{3.75}$ , with  $D \sim 80$  km. Here, groove lanes are  $20\text{--}120$  km wide with  $F \sim 100\text{ mW m}^{-2}$  and  $F \sim 50\text{ mW m}^{-2}$  outside this region, just below that inferred for dark terrain. In each successful case,  $\sim 50\%$  of the surface is under extension, consistent with proportionality of extensional grooved terrain and dark terrain. Convective downwelling regions remain stationary, allowing for the persistence of relatively undeformed terrain.

### 4. Discussion

Here we use a simple model to show that sluggish lid convection can provide the heat flux and strain rate inferred for grooved terrain formation. Calculations using more sophisticated plastic rheologies and in a spherical domain are required to test whether convection can create linear groove lanes. Viscosity dependent internal heating modes (e.g. Han and Showman, 2010) and the incorporation of damage or strain weakening (e.g. Buck et al., 2003; Bland et al., 2010) into convection models could be important in localizing surface deformation.

To form grooved terrain by convection, the upper surface must be sufficiently weak to allow convective plumes to come close to the surface. The effective yield stress of ice in tidally flexed ice shells may be low, as suggested by the presence of cycloids on Europa (Hoppa et al., 1999) and locations of tiger stripe plumes on Enceladus (Hurford et al., 2007), which both seem to be controlled by diurnal tidal stresses  $\sim 10\text{--}100$  kPa. Our results suggest a yield stress of this magnitude may permit convection-driven resurfacing, however this may require a coefficient of friction of

ice below the range suggested from laboratory experiments (Schulson and Fortt, 2012). Stresses from global surface expansion, which were likely important (Collins, 2008) may also have increased background extensional stresses and reduced the effective yield stress, allowing convection to drive deformation.

If the total extensional strain on Ganymede exceeds that from global expansion, convection was a likely driving force because passive spreading could not have driven deformation once expansion stresses had been alleviated. Estimates of the strain recorded in grooved terrain depend on the formation mechanism of subdued grooves (Collins, 2006), which could form by lithospheric spreading (Head, 2002) or cyovolcanism (Schenk et al., 2001). Abundant evidence for lithospheric spreading would imply a surface strain beyond what is possible (Collins, 2006) from differentiation and resonance (Squyres, 1980; Bland et al., 2009).

Dark terrain preserved above convective downwelling regions would have experienced significant contraction. Contraction has a variety of surface expressions, but by analogy with Europa, we expect long-wavelength compressional folds to form in the dark terrain (Prockter and Pappalardo, 2000; Pappalardo and Collins, 2005). Bland and McKinnon (2012) show that fold formation and lithospheric thickening on Europa can occur for strain rates of  $10^{-12}$ – $10^{-15}$  s<sup>-1</sup> and  $F \sim 20$ – $100$  mW m<sup>-2</sup>, close to conditions above convective downwelling regions in our models (see Fig. 3). No contractional features have been observed in dark terrain (Pappalardo et al., 2004) and deformed craters in dark terrain even show evidence for significant surface extension (Pappalardo and Collins, 2005). However, the presence of pervasive, long-wavelength and low-amplitude folds, would allow dark terrain to be regions of net contraction which accommodate extension in grooved terrain. Identification of long wavelength folds in dark terrain and crustal spreading along subdued grooves by ESA's upcoming JUICE mission would support convection-driven grooved terrain formation.

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